

DAVID W. TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER

Bethesda, Md. 20084

FINITE ELEMENT ANALYSIS OF THE ADP/COMMUNICATIONS SHELTER

bу

Petro Matula and Erwin A. Schroeder

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COMPUTATION, MATHEMATICS, AND LOGISTICS DEPARTMENT DEPARTMENTAL REPORT

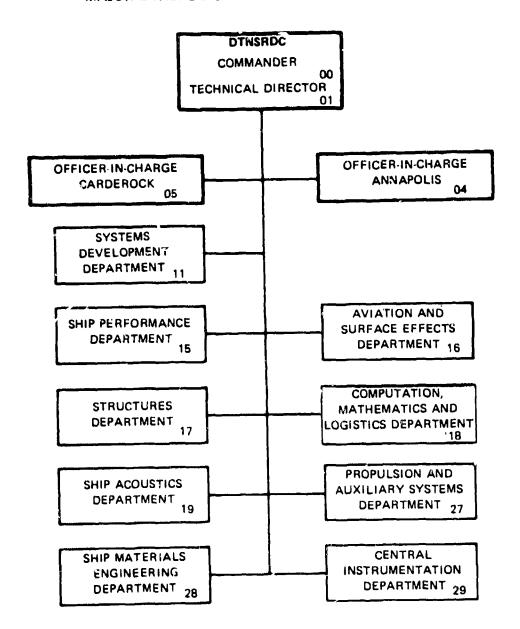
November 1978

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FINITE ELEMENT ANALYSIS OF THE ADP/COMMUNICATIONS SHELTER

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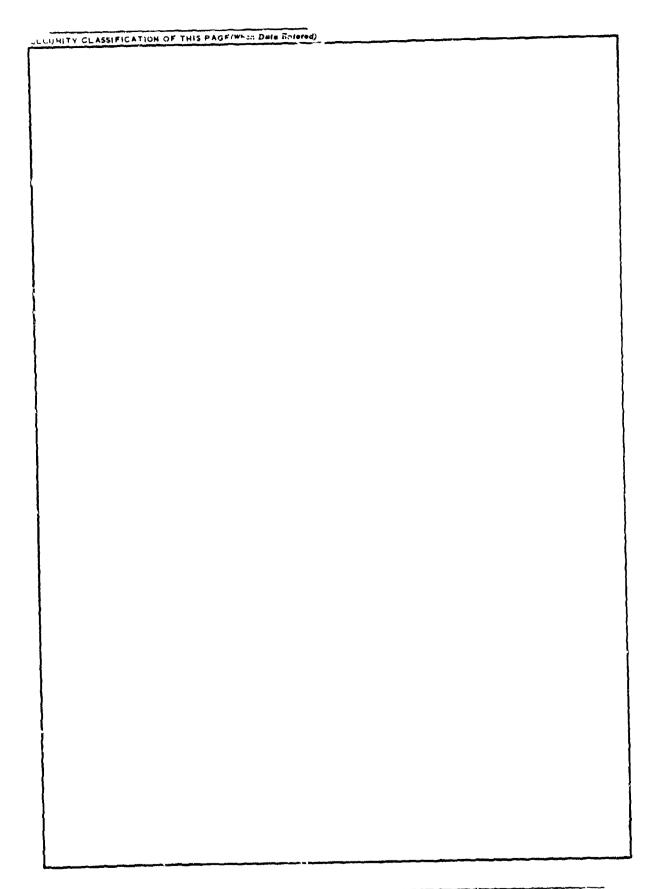
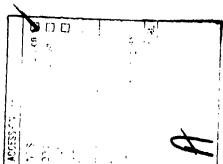


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ABSTRACT

The Navy NASTRAN Systems Office at the David W. Taylor Naval Ship Research and Development Center assisted the Naval Surface Weapons Center, Dahlgren Laboratory, in the structural analysis of the ADP/Communications portable computer shelter. The original and reinforced shelters were modeled with finite elements and the analysis was carried out using the computer program NASTRAN. The results of the analysis showed that the average stress in the floor of the shelter decreased 20% after the shelter had been reinforced.

ADMINISTRATIVE INFORMATION

This work was funded by the MAGIS office of the Naval Surface Weapons Center.

INTRODUCTION

The Navy NASTRAN Systems Office, Code 1844, of the David W. Taylor Naval Ship R&D Center (DTNSRDC) was requested by the Naval Surface Weapons Center (NSWC) to assist in the analysis of the ADP communications portable computer shelter (ADP/Comm shelter). The purpose of this analysis was to evaluate the shelter's structural strength when it is subjected to various loads as specified under its transportability requirements.

First, the original shelter was analyzed. Then NSWC reinforced the original shelter on the basis of the analysis results, and this modified shelter was analyzed anew.

In this report the term "original" shelter refers to the shelter design received by DTNSRDC for analysis. The term "modified" or "reinforced" shelter refers to the shelter which resulted from modification of the original shelter. (The floor of the original shelter had already been modified when the shelter was first received by DTNSRDC.)

The analysis was performed by the finite element method using the computer program NASTRAN.

This report describes the work performed.

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SHELTER DESCRIPTION

The shelter is an aluminum structure, approximately 8 feet wide by 20 feet long by 8 feet high (see Figure 1). It is made up of wall, roof, and floor panels. These six panels are joined along the edges to form the shelter enclosure. Figures 2, 3, and 4 show the connections between panels. The framework of these panels is made of tube beams with rectangular cross sections and with formed hat sections. The joists of the floor panel are braced with intercostals which also provide additional support to the floor. The floor panel is about four inches thick and is covered with aluminum skins 0.04 inches thick on the underside and 0.125 inches thick on the upper side. The roof and wall panels are about two inches thick and are covered with 0.04-inch thick aluminum skin. Approximately 1/4-inch thick wood spacers, as thermal insulation, are provided between the inner skin of the panel and its framework. The space between the skins in each panel is filled with a rigid foam insulation.

The shelter has a 3-ft. by 6-ft. main door located toward one end of one longitudinal wall and a 1.5-ft. by 6-ft. emergency door located in the other longitudinal wall diagonally opposite the main door.

The shelter has skid rails under the floor, wire rope sling attachments on the roof corners for helicopter lift and for tying down the shelter during rail transport, and pads and fittings at each end of the shelter for attachment of two-wheel trucks ("mobilizers") for road transportation.

The ADP equipment of the shelter is attached at strong points of the floor and the walls. Figure 5 shows an interior view of a partially equipped shelter.

STRUCTURAL AND EQUIPMENT MODIFICATIONS OF THE SHELTER

The general description of the shelter presented in the previous section applies to both the original and the modified shelters considered in this report. They differ only in details (described in this section.

As a result of the stress analysis of the original shelter NSWC strengthened the original shelter along corner joints and at the equipment attachment points. The modification of the corner joints can be seen in

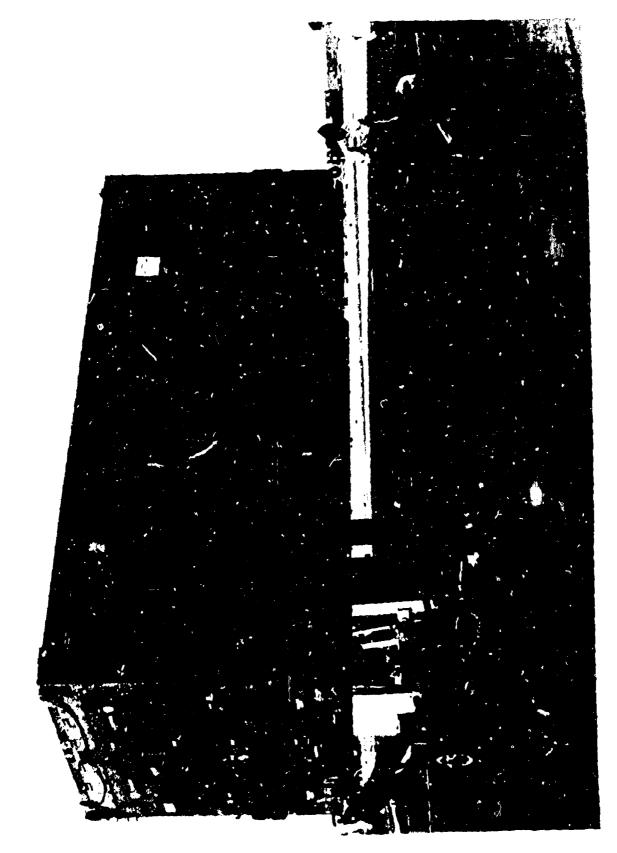


Figure 1 - ADP/Communications Shelter

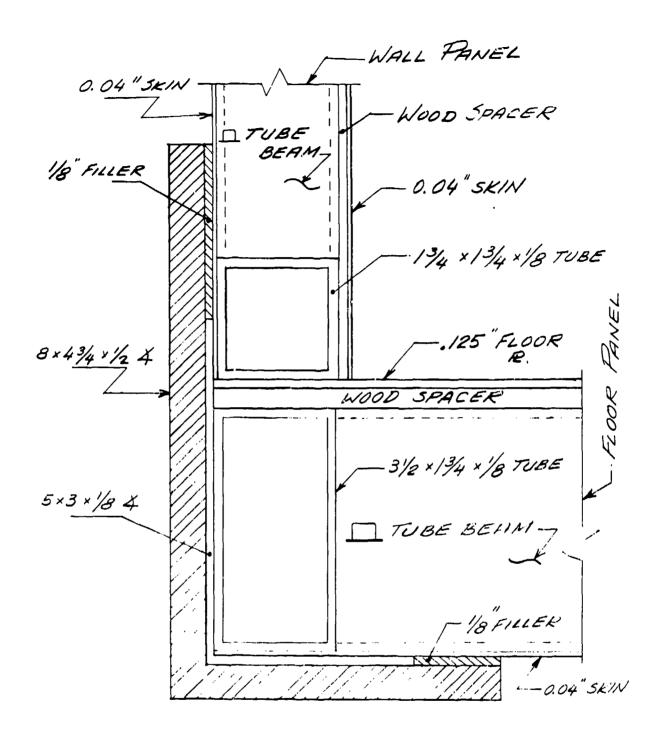


Figure 2 - Floor to Wall Joint, Reinforced (Shaded Parts are Reinforcements)

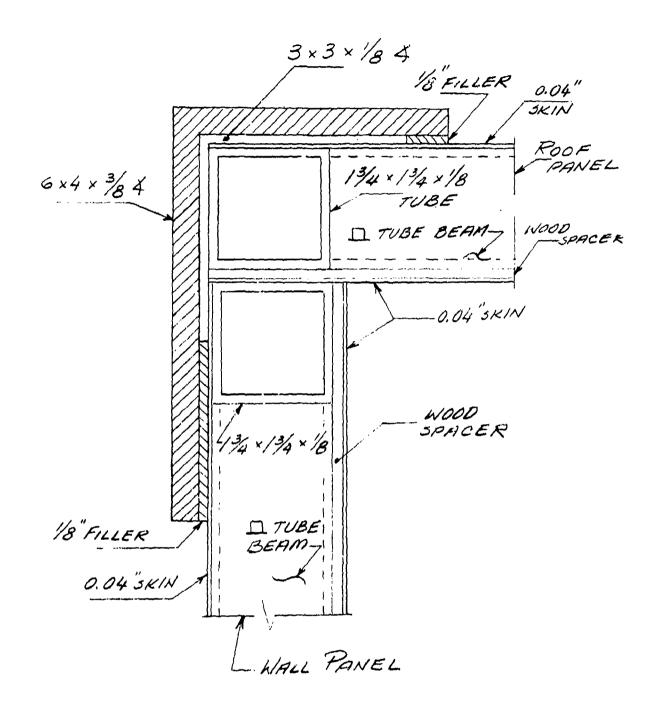


Figure 3 - Roof to Wall Joint, Reinforced (Typical, except Roof to A/C End Wall (see Fig. 6). Shaded Parts are Reinforcements.)

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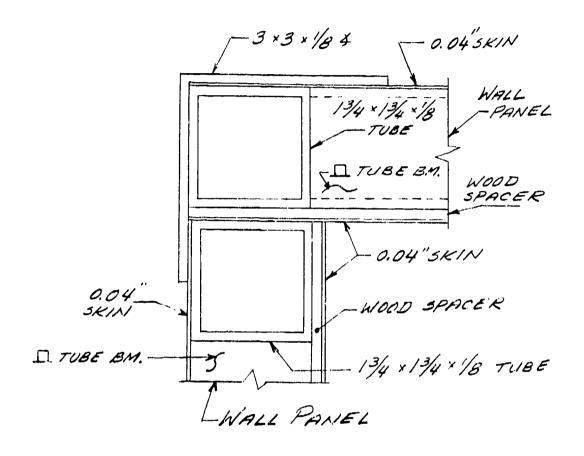
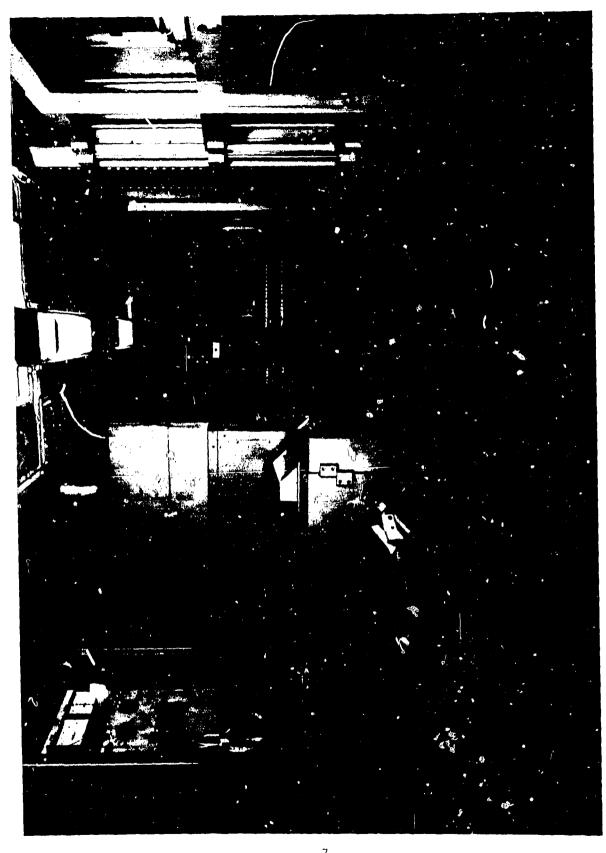


Figure 4 - Wall to Wall and Unreinforced Roof to Wall Joint



Figures 2 and 3; the 8 x 4 3/4 x 1/2-inch and 6 x 4 x 3/8-inch angles and the associated 1/8-inch filler plates are the additions (shown shaded) to the original corner joint configuration.

The equipment mounting points were reinforced by adding beams running transversely to and connected to floor joist beams and wall stud beams under and behind the equipment.

In addition to structural modifications, some of the internal equipment was relocated and its anchorages modified.

These changes were accounted for in the finite element model of the modified shelter.

FINITE ELEMENT MODEL

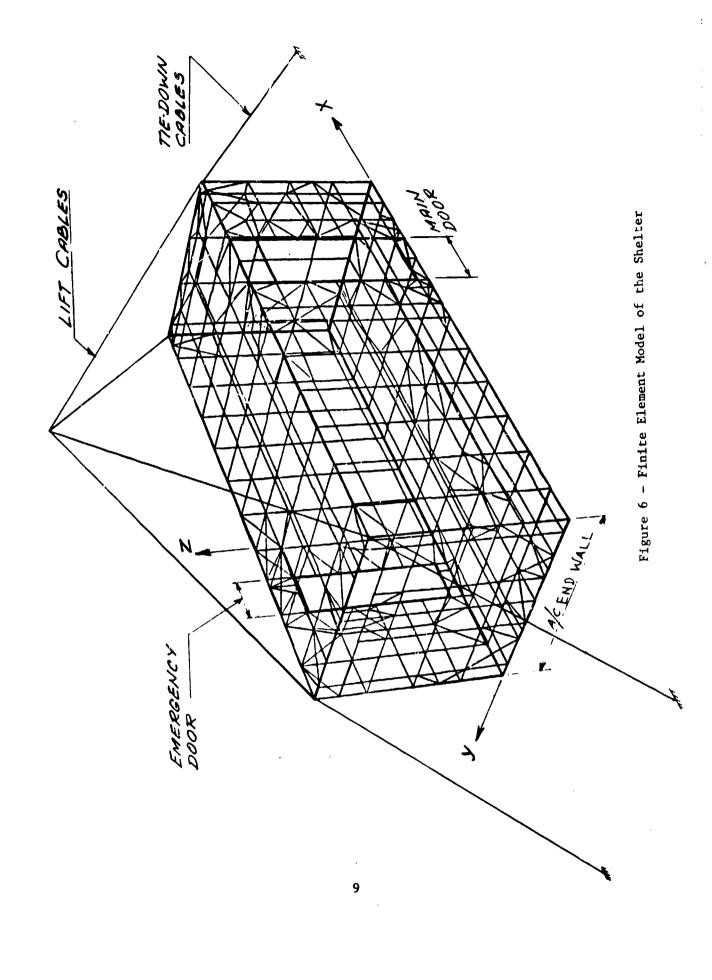
The finite element model of the shelter was produced by modeling each wall, roof, and floor panel with NASTRAN plate and beam elements. The complete finite element shelter model as plotted by NASTRAN is shown in Figure 6. The plate elements and the grid points of the finite element model are located on the neutral plane between the inner and the outer skins of each panel.

The shelter was modeled in a rectangular coordinate system with the origin at the point of intersection of neutral planes of the main door wall panel, the air conditioning (A/C) end wall panel, and the floor panel.

The plate elements used were the NASTRAN quadrilateral QUAD1 and triangular TRIA1 elements. Because these elements allow separate specification of plate properties for bending, shear, and membrane actions, they can be used to model the skins. The effective thickness for shear and membrane action is equal to the sum of the thicknesses of the inner and outer skins. The bending stiffness is computed by treating the ps all as a sandwich plate in which the two skins are separated by foam insulation.

It is assumed that the insulation between the skins prevents the skins from buckling but does not contribute directly to the strength of the panels.

NASTRAN's beam elements, BARs, run between the grid points. However, whenever a beam end does not coincide with a grid point, NASTRAN allows



specifying the offset for that beam end from its respective grid point.

Most of the beams of the shelter model are located at various offset distances from their respective grid points. Such offsets, however, do not show on plots done by NASTRAN plotting subroutines. Such plots show the BARs connecting grid points directly.

The tie down and helicopter lift wire rope cables are modeled with NASTRAN ROD elements. These elements possess axial and torsional stiffness only. For proper simulation of wire ropes the use of RODs in the shelter model is limited to axial tension.

The absence of bending stiffness in ROD elements made it possible to retain them in the finite element model even for those analyses which did not involve the cables. In such cases, the cables (RODs) were neutralized by a combination of proper boundary conditions and the absence of resistance in RODs in bending.

The ability to retain the same finite element model for various analysis conditions means that the stiffness matrix of the model did not have to be computed each time the cables were removed or added. This is important in reducing the cost of the analysis since the computation of the stiffness matrix is one of the more expensive computer operations.

The finite element model of the original shelter consists of:

- 382 grid points
- 2292 degrees of freedom (before constraints)
- 2210 degrees of freedom (after constraints)
- 218 rectangular plate elements, QUAD1
- 207 triangular plate elements, TRIA1
- 808 beam elements, BAR
 - 8 rod elements, ROD

and the complete finite element model of the reinforced shelter consists of:

- 384 grid points
- 2304 degrees of freedom (before constraints)
- 2121 degrees of freedom (after constraints)
 - 215 rectangular plate elements, QUAD1
- 211 triangular plate elements, TRIAL
- 877 beam elements, BAR
 - 8 rod elements, ROD

LOADS AND BOUNDARY CONDITIONS

The shelter is required to withstand several kinds of dynamic loads. However, the normal mode analysis results indicated that these dynamic conditions could be simulated by static loads as follows (see also Normal Mode Analysis section):

1. The Simulated "Rail Hump" - combines 20-g vertical and 30-g horizontal loads. The horizontal load acts along the longitudinal dimension of the shelter. With the vertical load acting upward, the horizontal load was allowed to act first on one end of the shelter and then on the other end, to provide for the possibility that either end of the shelter might be forward during a rail hump. The same two horizontal loads were applied with the vertical load acting downward. Thus there were four distinct cases to be analyzed.

With the vertical load in the upward direction, the shelter was constrained at the upper four corners by tie-down cables (Figure 6). With the load acting down, the shelter rested on the skid rails.

To resist the horizontal load the "front" lower edge of the shelter rested against blocking and was prevented from overturning by the two "rear" tie-down cables.

- 2. The flat drop condition was simulated by a 20-g load acting downward with the shelter resting on the skids.
- 3. The helicopter lift was simulated by a 4-g load acting downward with the shelter suspended by sling cables attached to the four upper corners (Figure 6).

NORMAL MODE ANALYSIS

The shelter was analyzed for normal modes below 50 hertz. For this analysis the shelter was modeled as supported at the mobilizer attachment points to simulate the boundary conditions during ground transportation.

The results were compared by NSWC with shelter dynamic test data as well as with the specified time-dependent load functions to assure adequate separation of normal and input frequencies to avoid resonance.

The information thus derived helped to specify a static design load in place of a dynamic condition. The frequency of the fundamental mode of the original shelter was found to be 11.5 hertz. The vibration mode corresponding to this frequency is shown in Figure 7.

NASTRAN OUTPUT DESCRIPTION

Pages 18 through 33 contain samples of NASTRAN shelter analysis output, which consists of two parts: (1) complete listing of the input data, and (2) analysis results as requested. The parts are described in this section.

INPUT DATA

The input data listing is grouped as follows:

- a. <u>Executive Control Deck</u>, page 18, defines the job and the type of analysis to be performed as well as many other conditions and requirements that a user may specify for his job.
- b. <u>Case Control Deck</u>, page 19, defines a subcase structure for the problems, selects data from the Bulk Data Deck, and requests printed, punched, or plotted output. The Case Control Deck of the shelter problem contains six subcases. Each subcase specifies one of the prescribed load conditions for analysis as labeled. These labels and subcase numbers in the input data are used to identify the pages of analysis output.
- c. <u>Bulk Data Deck</u>, beginning on page 20, is the primary NASTRAN input. This deck defines the structural model and various pools of data which may be selected by case control at execution time.

The shelter structure and the data for analyzing it are specified by the following alphabetically listed cards. For the specific format and requirements of the data cards, see the NASTRAN Users' Manual.

CBA' gives the grid point connections for the beam element, BAR, with acial, bending, torsional, and shear stiffness.

CONM2 concentrated mass used to represent the mass of internal equipment.

^{1 &}quot;The NASTRAN Users' Manual," NASA SP-222 (03), National Aeronautics and Space Administration, Washington, D.C. (1976).

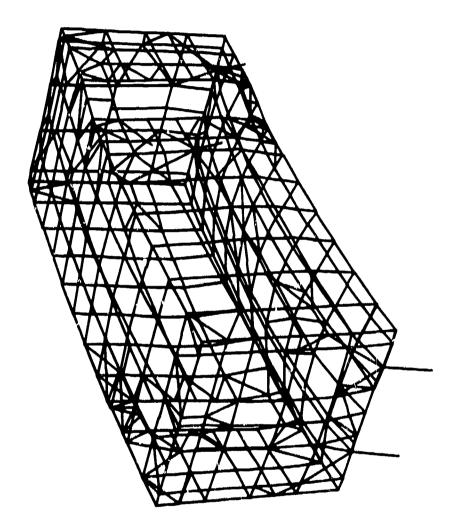


Figure 7 - Fundamental Vibration Mode of the Shelter

CQUAD1 connections for rectangular place elements that represent the two skins on the panels.

CQUAD2 connections for rectangular plate elements used to represent panels.

CRIGD1 defines rigid connections between internal components of the shelter.

CRIGD2 rigid connections that represent mounting of the two doors by hinges and latches.

CROD connections for rod elements that are given only axial stiffness.

Used to represent tie-down and lift cables.

CTRIAL connections for triangular plate elements that represent the two skins.

DEFORM defines an initial deformation. Used to represent prestress in the tie-down cables.

EIGR specifies the range of natural frequencies to be computed.

GRAV specifies gravity type loads to represent the various types of loads on the shelter.

GRID defines the identification number of a grid point and specifies its coordinates.

LOAD defines combinations of the gravity loads given on the GRAV cards that represent the various loads applied to the shelter.

MAT1 specifies structural material properties.

MPC defines a linear equation between specified degrees of freedom.

PBAR defines beam properties for the BAR elements.

PQUAD1, PQUAD2, define plate properties for the QUAD1, QUAD2, TRIA1 elements. PTRIA1

PROD defines properties for the kor alement.

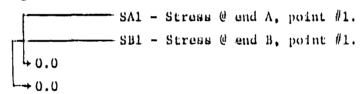
SEQGP Input data was produced by BANDIT, a program that is a preprocessor to NASTRAN. BANDIT resequences the original numbering of grid points to minimize matrix solution time, page 25.

SPC1 | define boundary conditions.

ANALYSIS RESULTS

Samples of shelter analysis output data are shown on pages 27-33. Each page of the output is identified by the subcase label and the subcase number.

- a. <u>Displacement Vector</u>, page 27, shows displacements of each grid point under the loading specified in the subcase shown at the top of the page. T1,T2, and T3 are translations, in inches, along the x-, y-, and z-axes, respectively. R1,R2, and R3 are rotations, in radians, about the x-, y-, and z-axes, respectively.
- b. <u>Load Vector</u>, page 28, shows the loads at each grid point resulting from the applied gravity action. T1,T2, and T3 are loads acting along the x-, y-, and z-axes, respectively. R1,R2, and R3 are moments acting about the x-, y-, and z-axes, respectively.
- c. Forces of Single-Point Constraint, page 29, show force reactions of the constrained grid points. T1,T2, and T3 are force reactions acting along the x-, y-, and z-axes, respectively. R1,R2, and R3 are moment reactions acting about the x-, y-, and z-axes, respectively.
- d. Stresses in Bar Elements (BAR), page 32. NASTRAN provides for obtaining stresses at up to four points on the end cross-section of a bar element. The first column in this output gives element 1D number. The next four columns show the stresses at the eight specified points for each bar element arranged as follows:



etc.

The sixth column shows the axial stress. The last two columns give maximum and minimum stresses at ends A and B. These stresses are obtained by adding the axial stress (col. 6) and the maximum positive bending stress at one of eight specified points to produce "MAX.", and the axial stress plus the highest negative bending stress for "MIN.".

e. Stresses in General Quadrilateral Elements (QUAD1), page 33. Columns 3, 4, and 5 show stresses in plate elements in the element

coordinate system. The plate element coordinate system in NASTRAN is established on CQUAD and CTRIA cards as follows: the origin is at the first grid point listed on the card. The x-axis goes through the second listed point. The y- and z-axes are then added according to the right-hand rule. Columns 6, 7, 8, and 9 show principal stresses as computed from the stresses in columns 3, 4, and 5. QUAD1 element ID numbers are listed in Column 1. Column 2 shows the distance from the neutral plane to the fibers at which the stress was requested. The fiber distance is in the element coordinate system.

RESULTS OF THE ANALYSIS

After the original shelter was modeled and analyzed, it was reinforced and the internal equipment and its supports were rearranged. The analysis process was then repeated on the modified shelter.

The reinforcements consisted mainly of additional floor and wall beams for equipment mounting and strengthened joints between the floor and the walls.

The finite element model was changed to reflect these modifications in the shelter and equipment configuration. These reinforcements changed the original finite element model by the shelter sufficiently to preclude accurate point-by-point comparison of stresses between the two shelters. However, for an analysis of a rail hump—the most severe of the tests—the average of the stresses in the internal floor beams was computed and found to decrease by 20% after reinforcements to the shelter were incorporated in the finite element model.

ACKNOWLEDGMENTS

We acknowledge the help of Suzanne Wybraniec who took an active interest in preparing and checking the NASTRAN input data and tabulating the stress output. Michael Golden wrote a computer program that expedited punching the large number of data cards needed to model the shelter. We also thank Dr. S. K. Dhir for his interest and helpful suggestions.

APPENDIX NASTRAN SAMPLE* DATA AND OUTPUT

*NOTE: The complete NASTRAN output set is available from Dr. C. Blackmon, Code K21, NSWC, Dahlgren, Virginia 22448.

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DIAG 1.6.19.22
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\$GRID 400
\$CCNFIG 6
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CHKPNT FES,DISK
APP DISFL
SQL 1.0
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422-	SEGGP	10864	52	10843	98	10677	23	13343	97	
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312101	U	-3.431760E-02	-9.687600E-02	1.221971E+30	-1.246282E-02	-6.488247E-04	
312487	g	-1.534341E-01	1.210732E+00	1.325923E+50	-9.304279E-03	-2.938839E-03	-1-25005E-03
**	g	-3.2765:85-02	-9.437229E-02	1.1116E6E+C0	-1.591/8GE-02	-2.478344E-U3	#0-20ft 650 - B1
	g	-2.773353E-02	-9.05427CE-02	8.2759736-01	-2.066284E-02	Z.038006E-03	Z. 126366E-04
314787	وي	-1.1693538-01	1.210425E+00	1.022698E+00	-1.708334E-02		-1.584143E-03
316501	IJ	-2.046355E-02		3.983742E-01	-1.877502E-02	5.38c406E-03	-1.489224E-03
317001	g	-1.452575E-02	-8.8258C6E-02	3.043134E-01	-1.686384E-02	5.459534E-03	-7.491630E-04
317087	G	-7.823700E-02			-2.443430E-02	-8.227764E-04	-1.879744E-03
318601	6	-5.436300E-63	-8.918445E-02	8.783690E-02	-1.326720E-02	2.5913236-03	-1.3297296-03
319301	ی	-1.345437E-03		٠	-1.403723E-02	3.040978E-03	-1.329268E-03
319307	J	7.2845905-03	-6.142890E-03	-1.334557E-02	-1.346598E-02	4.331475E-03	-2.048734E-03
319375	U	-5.295089E-02	9.636831E-01		-1.788023E-02	3.488055E-93	-2.9391715-03
319387	وي	-3.551945E-02	1.219815E+00		-2-212142E-02	2.570391E-03	-1.35/639E-03
349301	<u>.</u>	-1.517047E-C3	-9.617621E-02	٠	-1.447973E-02	Z.240331E-03	-1./00839E-03
349327	g	1.2166945-03	-1-859515E-02	-3.225844E-02	-1.139945E-02	1.979236E-03	-4. 363630E-03
349322) ق	-1.100588E-02	1.534376E-01	-4.295155E-02	-1.256550E-02	-1.3/1308E-03	-2.069201C-03
349333	، ق	-1.7367C6E-02	3.045532E-01	-4-64-6636-02		-1.1333/3E-03	•
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349387	ט פ	-3.5749235-02	1.204496E+00	-3.288099E-02	-2.283055E-02	2.136934E-03	-1.471825E-03
420101	U	-6.694687E-02	-1.311791E-01	1.535939E+00	-1.475584E-02	-8.371609E-04	-1.288157E-03
420122	U	-9.842921E-02	2.058357E-01	1.542C12E+00	-1.616E32E-02	-1.531745E-03	-1.982229E-03
420143	ڻ	-1.287836E-C1	5.529274E-01	1.545984E+00	-1.631350E-02	-1.656137E-03	-2.719831E-03
420164	IJ	-1.557835E-01	8.9953855-01	1.548228E+00	٠	-1.066392E-03	-2.491359E-03
420187	ڻ ا	-1.795CS1E-01		1.548385E+00	-8-794426E-03	-1.096890E-03	-1.43/2005-03
420801	יט	-5.703E52E-02	-1,308161E-01	1.4316895+00	-1.3/15826-02	14.375090E-04	
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422487	ט נ	-1.4700046-01	1.1.86625+00	1257565400	-1 BAG 130F-03	-2 0075195-03	-8.385317E-04
422301	ט פ	-4.6/3320E-02	10-3/10/10/10	8.5715895-01	-2.456196E-02	3.434127E-04	-9.051549E-04
424787	ی د	-1.1357385-01	1.178110E+03		-1.7394:5E-02	-3.202316E-03	-1.453811E-03
426501	U	-3-203689E-C2	-1.2421136-01	2.983321E-01	-1.876074E-02	2.686528E-03	1.298891E-03
427001	U	-2.631405E-02	-1.2-2732E-01	2.1633895-01	-1-436934E-02	.757184E-	-1.402210E-03
427037	ڻ	-7.673939E-02	1.17E124E+00	5.7109635-31	-2.691578E-02	-2.203031E-03	-1.670493E-03
428501	ٯ	-6.7244405-03	-1.210171E-01	3.920771E-02	-1.025336E-02	Z.605431E-03	-1.845575E-03
N	U ·	-2.770144E-03	-1.234339E-01		-1.108749E-02	1,298423E-03	-9.461613E-04
429322	IJ	-8.761490E-GG	10-3656310	-4. 433953E-12	-1.063735E-02	-1.022575E-03	-3.938017E-03
429343	ڻ	-2.448243E-02	3.624037E-01	٠	-1.432051E-02	-1.470704E-04	-6.541363E-03
429364	ق	-3.E32279E-62	7.CC9693E-01	-4.7212495-52	-1.764876E-02	-4.470463E-04	-5.395932E-03
429375	ی	-4.034970E-02	8.9533318-01		-2.014254E-02		-3. 726228E-03
429387	U	-3.645544E-02	1.17E465E+00	-5.067415E-02	-2.463908E-02	B. 209671E-04	-1.811909E-03
530101	<u>.</u>	-7.681C38E-02	-1.539298E-01	00+3610136-1	-1.346361t-02	-8.072583E-04	-1.1119605-03
530122	، ق	-1.037228E-01	1.651050E-01	1.36:0355+09	-1.550142t-02	-1.436200E-03	-1.3/8304E-03
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530164	ט פ	-1.5455888F-01	# 1400F00F101	1.300002E+30	-1 -60-1535-03 -5 705242E-03	-7 605042E-04	-1 306502F-03
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532101	9 (9	-5.820433E-02		1.282533E+C0	-1.6731055-02	-1.354891E-03	-2.685693E-04

LOAD VECTO

11	-1.642638E+02	0.0	2.405021E+00	D (D		0.0	0.0	4.913467E+00	-1.784595E+02	0-0	0.0	9.128002E+01	0.0	3.569189E+02	-4.381338E+02	-3.634663E+02	0.0	-1.405102E+02	0.0	0.0	2.828066E+02	4.292969E+02	0.0	-8.450140E+01	o.0	0.0	0.0	9.0	0.0	-3.439271E+02	0.0	0.0	1.825600E+02	0.0	3.569189E+02	3.3614346402	-3.150200E+VZ	0.00	-1.40510ZE+0Z	0.0	0.0	5.656132E+02	8.470199E+02	0.0	-3.492312E+01	0.0	0.0	0.0	0.0
R2	1.485356E+02	1.806386E+00	-4.221281E+00	-Z-Z78011E+01	-1.800714E+01	-1-822409E+01	-1.844104E+01	-1.600714E+01	-5.301280E+01	1.504202E+02	2.976584E+01	0.0	-5.434128E+02	0,0	3.227440E+02	2.924425E+02	-5.479757E+01	0.0	-3.573699E+02	9.200627E+01	4.787348E+02	5.452513E+01	-2.360498E+02	0.0	1.797938E+02	2.872638E+01	0.0	0.0	<u>.</u> د	0.0	4.815922E+02	2.976584E+01	0.0	-1.086826E+03	0.0	3.227440E+02	2.803332E+02	6.000488E+U1	0.0	-3.694572E+02	9.200627E+01	2.393674E+02	-2.350105E+02	-2.239625E+02	0-0	4.335100E+01	3.018834E+01	0.0	0.0	0.0
ž	-1.095092E+02	0.0	1.603347E+00	0.0	0.0	0.0	0.0	0.0	3.275644E+00	-1.189730E+02	0-0	0-0	6.035335E+01	0-0	n.	-2-920E =+02	-2.4231C3E+02	0.0	-9.367349E+01	0-0	٠ <u>٠</u>	1.885377E+02	2.861980E+02	0.0	-5.633426E+01	0.0	0.0	0.5	0.0	0.0	-2.297848E+02	6 (0.0	1.217067E+02	0.0	2.379459E+02	70+3697467-7-	-2-1200045±02	D . 5	-9.367349E+01	ت ت	0.0	3.7707556+02	5.646799E+02	0-0	-2.328208E+01	9.0	0 0	0.0	0.0
13	2.072448E+02	1.739747E+02	1.443996E+02	9.203337E+01	1.302513E+02	B. 928977E+01	1.333839E+02	7.2801335+01	1.51626EE+32	2.384226E+02	4.713211E+02	3.966954E+02	4.332773E+02	4.061384E+02	5.634181E+32	7.4652795+02	4.937631E+02	C.525652E+02	6.3647315+52	7.091152E+02	4.330638E+32	1.495520E+03	4.705251E+02	3.694549E+02	8.223485E+02	4.133360E+02	4.052897E+02	4.013335E+02	2.883438E+32	2.038975E+02	4.136151E+02	4.713211E+02	3.67167CE+02	5.C59C77E+02	4.042CB1E+02	5.6575748+92	2.331.258E+32	2 060303036-02	3. 3323035402	5.5307196-02	7.09:152E+02	4.795733E+02	1.295516E+03	5.183253E+02	3.9657485+02	8.174839E+02	4.747343E+02	3.963432E+02	3.9882635+02	4.0315132+02
12	0-0	0.0	0.0	0.0	0.0	0-0	0.0	0.0	0-0	0.0	0-0	0.0	0-0	0.0	0.0	0-0	0.0	0 -د	0.0	0.0	0.0	0.0	0-0	0.0	0.0	0.0	0 .0	٥.5	٥.٥	٥-° ٥-°	0.0	0.0	0,0	0-0	හ - ප -	۵. د د		5 c	3 (0.0	۵- ۵-	0.0	0.0	0.0	o-0	0 .0	ڻ. 0	0.0	0-0	0
11	٠		٠		-1.953770E+02	٠		•		-3.576339E+02			•	•		•	-7.406521E+02		٠		•	-2.2.3729E+03	•			٠			-4.325112E+02	-3.058463E+02	-6.204227E+02	-7.069816E+02	-5.506605E+02	-7.583615E+02	-6.053121E+02	٠	٠		٠	i	-1.063673E+03		٠		-5.950122E+02	٠	-7.121015E+02		-5.832395E+02	-6. 047270E+02
TYPE	v	IJ	U	ט	ت	ی	g	U	b	ی	ق	ی	U	IJ	U	G	U	IJ	ي	G	ی	G	ڻ	U	IJ	IJ	IJ	G	G	٠	۰	۳	ت	U	ڻ ا	ن ق) و) و	9 (٠ ق	IJ	G	ß	U	IJ	U	و	U	U	U
POINT ID.	319387	349301	349307	349322	349333	349343	349354	349364	349375	349387	420101	420122	420143	420164	420187	423801	422101	422487	422901	424101	424787	426501	427001	427087	428601	429301	429322	429343	429364	429375	429387	530101	530122	530143	530164	530187	536831	532101	2324B/	532901	534101	:34787	536501	537061	537087	538601	539301	539322	539343	539364

L HIMP-A/C END FORMARD-VERTICAL ACCELERATION UPWA

ភូ	4.0301695-23	8.058557E-25	-9.815156E-24	B.032999E-24	6.988594E-24	-1.026526E-24	2.165398E-23	-9.328127E-06	-2.634878E+06	3.292709E-23	9.283368E-14	9.180990E-24	-7.520430E-08	-6.121689E-26	-1.378939E-07	-5.2869335-25	-2.801517E-08	4.829779E-24	2.351590E-08	1.262247E-26	7.303242E-10	1.216449E-09	0.0	0.0	0.0	0.0	0 -0	0.0	0.0	0.0	1.210719E-08	1.117567E-08	1-490115E-07	-2.682209E-07	0.0	9.0	9	0.0	0.0	0.0	0.0	٥-٥	0.0	0-0	0.0	0.0	0.0	0.0
R 2	4.447979E-23	-3.515788E-24	1.361726E-24	-5.135622E-23	-1.413944E-23	-4.280845E-24	1.473857E-23	0-0	1.545262E+06	3.192287E-24	-5.855013E-24	3.603296E-24	0.0	-1.432398E-25	0.0	-7.743020E-26	0.0	-2.176759E-24	0.0	7.263280E-26	0.0	0.0	0.0	9.0	0.0	0-0	0.0	9.0	0-0	0.0	٥.٥	0.0	0-0	0.0	0-0	6.9	- c	0-0	0.0	0.0	0-0	0.0	0.0	5.3931235+03	-2.8471936+03	1.108647E+04	3.843506E+02	7.451113E+03
Z	1.519447E-22	3.6837085-23	2.688234E-23	E.543753E-23	2.788436E-23	2.642347E-23	1.201217E-22	0-0	8.268149£+05	3.169464E-25	6.055888E-23	1.011156E-22	0.0	6.9991991-25	0.0	7.503926E-25	0.0	2.658011E-23	0.0	6.716883E-25	0.0	0-0	0.0	0.0	٥-٥	0.0	0 -0	0.0	0,0	o. o	0.0	0.0	0,0	<u>ت</u>	0 .0	0.0	٠ ت	ن -	0-0	0.0	٥-٥	٥.0	9-0	0.0	0.0	0,0	٥.	0.0
1	0-0	0-0	010	9-0	. 0.0	0-0	0.0	0-0	0.0	0.0	6.0	0.0	0.0	0.0	0.0	0-0	د.ه	0-0	0.0	0.0	0.0	0.0	0.0	0.c	0.0	o. 0	-3.C05745E+04	-2.453347E+02	-3.259250E+34	3.535330E+03	0.0	0	0-0	<u>ن</u>	0.0	o-0	ت د	ن -	0	٥.٥	0.0	ت.	0.0	0.0	0-0	0-0	0 -0	0.0
5	0,0	0,0	0,0	0,0	0.0	0.0	0.0	9-0	0.0	0.0	0.0	0 .0	0 .0	0.0	0.0	<u>.</u> و. د	0.0	0.0	0 .0	0°5	0.0	0.0	0.0	-4.456524E-11	-2.910383E-11	-1.455192E-11	9 .0	ن د	0,0	0.0	0.0	ڻ ت	0-0	0.0	3.393314E+04	o-0	3 '3	0,0	0	٥.۵	ن .	ن .0	o.c	o.c	٥. د	0 0	0.0	0.0
11	. 0.0	0-0	0	0-0	0.0	0-0	0.0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.0	0-0	0.0	0.0	0-0	0.0	0.0	0.0	-5.820766E-11	8.185452E-11	1.74523GE-10	0.0	-1.923649E+04	-1.570120E+02	2.084387E+04	-2.260986E+03	0.0	0.0	0-0	۵. ۵	8.042356E+64	9.6850516+04	1.5979646+03	-6.843198€+04	:.974032E+04	-2.899736E+04	8.190112E+04	1.3:1317E+04	-8.268686E+03	0.0	0.0	0.0	O.0	0.0
TYPE	ی	U	J	.	ט פ	U	ט	G	6	ی د	ש	ש	ש	U	ט	ש	U	יט	U	U	IJ	U	ø	IJ	ט	()	ij	IJ	IJ	ق	ق	ق	IJ	U	_U	U	•	IJ	Ģ	IJ	ט	IJ	IJ	Ø	G	؈	Ç	ڧ
POINT 1D.	_	7	m	•	60	Œ	Ę	*	5	9	17	9	2	7	22	23	7	, %	12	78	29	ě	नि	æ	H	*	ŝ	ß	57	87,	61	8	B	4	10101	10801	10-52	13301	14701	16061	16501	18601	19301	169331	169343	169354	1010131	1010143

ICES IN BAR ELEKENTS

	TOROUE		7	7	φ	7	F	7	.	m 4	٠ ا	<u>.</u>	; ·	; ·	; ;	r ·	.+02 -3.309128E-V		.	103 -1 055434F-0	9		ųi m	+63 4.630766E-0	3 7.	3 -2.		ei (P	;	; ·	.+02 4.630/66ET	: 7		m	+03 6.386042E+0	+03 2.898269E+0	-	æj ·	7	ņi (ŇI	•	+02 -3.29023/E+0	- 6	7. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	i y	'n	
AXTAL	FURCE	1.962752E+03	-4.182961E+03	-1.843393E+03	-3.136241E+03	-3.199385E+03	1.754799E+02	2.790116E+02	-6.765429E+02	-1.015123E+0	-4.0838382+02	-1.622739E+03	1.285927E+04	9.433274E+03	-2.689935E+03	-2.570655E+03	-4.416506E+02	1.020219	6.699 519E+02	CONTRACTOR AND CONTRACTOR	: 631647F+0	-4 OC4946F40	-1.957135E+03		-1.821359E+0	4-097636E+0	-1.682284E+0	1.074417E+0	5.942758E+0	1.380078E+0	9.216/89E+01	-3.627.199E+02	1 0373055104	1.394590F+03	-8.493881E+C2	-2.207747E+03	-4.535652E+03	-4.170038E+01	-6.396947E+02	4.102332E+03	2.342069E+02	3.945960E+03	2.3/434/2403	2. 66328E+02	2.3180926	1.3531235+03	504719854C.1	7.122229E+02	
SHEAP -	DI SNE 3	ï		01 8.8533296+01	7		?	•	'n		- (N	¥ '	- (M) ('n	ni q	9 (62 -2.291063E+01	•	. (2		1	_	7	7	7	1	-		M (02 1.6453C1E+00	•	- M		-	02 2.380546E+01	CO 2.916438E+01	ያ)	m (ľ	اظ	9	7 +	~ (01 9.320884E+01	- 4	j -	
1	DI AVE 1	2 -R 339051F+01	3 2.857380E+02	3 3.C17273E+91	3 -3.7444CGE+C2	9-139096	m m	=	3 1.3395516+02	3 -3.366270E+02	3 -4.0/36332+02	1 -2,161235	2_016338	.	N	1	2 -2.402380E+50		2 -2.2383125+02	20.50015E005.2.2.	1 599414F+G2	CENTROPICATION A C		1- 1	2 1.	ťV	4 -2.090180E+0;	1	י מנ	N (2 3.4164.42E+01	20+35:0:32:11	201101 - 1 101101 - 1	3 -7 *540305+01	2 1.613437E+01	± 2.527328E+C2	4 5.6140105+02	3 -6.994432E+CO	e e	1	φ' (m) (2 -1.8351445+01	3 85 C34200E+	10+310*01*0 7	- +	. 6	
FWT CLY-B		11751-1-		2 -1.252401E+C;	3 2.757454E+C;	٣	-	14	-	3 -3.020474E+C;	3 1-8392245+0	2 -6-432858E+C	4 -3.5463345+03	3 1.165714E+C2	2 -5-7027-95-0	3 -8-6351236+62	1 -2.962521E+C2	73+307007-9	3 -2-34/032E+02	うしいけっからしゃ しゅう	4	7 4	. M	3 -5.7189338+0	3 1.772355E+C;	3 -4.6397368+0;	2 -1.623836E+0:	2 -3.5845695+0	2 -1.4453316+03	2 -7.315193E+01	2 -4.771167E+C	3 4.757251E+0	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	10+3115dbT e- 8	2 -1 -634337F+C	3 -1.331151E+C-	2 -1.2863325+0	1 -1.8735185+0.	2 8-3651355+60	3 2-420142	2 -1.609235E+C	3 1.748139E+C	3 3-395248E+0	2 6.2242445+C	3 3.001030E+C	; ;	i	3 -5.3731185+62	
RENO-WORKS	DI ANE 1	4 51122FF+C3	-4_096272E+03	-3.6C7934E+C2	1.025873E+C;	-6.7521E8E+C	1.192495E+C2	-2_C76292E+03	-2.944791E+C2	3.291833E+C	3.14.322E+3.	7.362562E+C	-1.0821845+5	0-6.643834E+C	-9.37765CE+C	1.225535E+C	-5.928837E+0	111111111111111111111111111111111111111	Z-355571E+0	A STREET OF ST	10-331122C-0-	0 1155 C 1155 C 1	-1 244797F+C	1.286393E+0	-1,569449E+0	-1,47E339E+G	7,15943355+0	4.3048408-4	-3.58337EE+C	-2.572477E+C	-1.582965E+G	1.2863902+0	Stantanon"	3 573700F	-1.C157CEE+5	-2.932435E+C	-4.735271E+C	6.1924245+0	-3.333828E+C	1.852353E+C	-1.016933E+C	1	-2.932831E+C	3,3779368+6	-2.43233985+0		-4.23/23/2+02 -1.03/20/00/100	-1.010976E+03	
A-CW3 TA		Œ		6.854416E+02	-1.4556735+03	3.540976E+02	-2.665282E+02	2.34:693E+02	9-146159E+02		-9.692252E+02	-5.021555+02	7.281476E+33	3.890945E+03	1.8345635452				-7.937209E+62	70-1204-100-1-	7 130216F+03		-6. F94237E+02		-2.617632E+C2	4.421645E+C2	-3.808772E+03	-5.0546655+03	2.720445E+03			7.6415735405	-3.6224256+30	-7 10EBBGE-00		-4.192671E+03	-1.267052E+C4	-1.197800E+C3	.259360	1.8147335+04	-2.1168785+03	2.10210CE+04		-1.011917E+03	. 38905C	1.2/2653E+43	-1.21E509E+US	-8.45c522E+02	
TWO MENTAL STATES	DI ANT	-3 R27R23E+03	2.1899545+03	3.03505E+02	-7.211656E+03	1.3353822+03	1.716431E+62	1.192435E+02	1-395034E+03	-4.113965E+03	-5-815110E+03	2-625059E+02	3.3537606+04	5.997269E+03	4.925555E+03	-1.07112E+03	-1.121457E+32	-7 -335 / 35E+03	-2.528435E+03	53+305+305.2- 6 600000000000000000000000000000000000	- 0 - 3303000 - 0 - 0 - 0 - 0 - 0 - 0 -	SON DESCRIPTION OF THE PROPERTY OF THE PROPERT	-1 780751E+02	-1.045241E+03	1.623626E+03	5.167319E+02	-1.792273E+03	-4.210422E+02	8.632539E+02	2.352741E+02	5.933:90E+02	-1.045341E+03	1-6235265+03	-1 -0:4403E+03 -1 - 685031E+03	1.3151005+02	4.718752E+62	4.085519E+03	-1.015706E+02	-9.450041E+02	-3.333928E+02	-2.113933E+02	-2.765216E+03	4.358872E+03	-1.0:6933E+02	3.386772E+03	1.159456E+03	-1.750551E+02	4.8322U5E+02	
Es cuckt		, e . e .	660800	662100	662930	669386	690053	690067	6900E1	208069	692900	694787	696530	697000	698600	000069	10269	86.669	99326	#/ Phino	707770	100001	710001	710046	710075	720087	720100	720187	726500	727000	728600	730046	733075	750400	751287	75:400	752500	753587	753800	755600	755837	756700	757800	758187	758900	759311	759332	759375	

HIMP-A/C END FORMARD-YERTICAL ACCELERATION UPSARD

Current	*	-3.339428E-03	-5.869985E+01	٠	٠	1.04368/E+01	-1 880305E+03	-3.089182E+00	-1.925420E+02	-4.381444E+01	-2.054289E+01	1.418979E+01	٠	9.162887E+00	3.844676E+01	1.137652E+31	1.488482E+01	-2.533430E+01	Z. 393251E+01	-9.414675E+01	-1.390799E+02	9.95062BE-01	-8.747457E+01	7 7667876460	7 183080E+01	1 \$40498F+03	-3.059704E+01	2.466329E+02	-1.178987E+00	1.492827E+01	2.939297E+00	6.268049E+00	5.211856E+00	-2.387236E+01	1.484/335+01	-6.140690E+0d	3,4359656+00	-2.558069E+01	6.294901E+00	1.746444E+01	-7.108563E+00	5.378984E+01	6.755495E+01	6.705635E+01	-3.154060E+02	-2.824352E+02	-1.114462E+02	2.225560E+01
	W K	9-4707-46+60	1.612326E+01	-8.113318E+01	4.316210E+01	-3.773558E+00	20-130-150-150-150-150-150-150-150-150-150-15	-2-857242F+00	-3.978531E+02	4.433300E+01	1.907079E+00	-3.316219E+02	-8.529372E+00	-9.385661E+00	-3.202831E+01	1.093423E+00	2.264213E+00	6-409290E+00	1.0420336+01	-5.986642E+01	-6.993535E+03	-2.868301E+00	1.504759E+02	70431467467	7 87 58 35 5 40 4	1 450935F-61	5.2019696+00	-4.844518E+02	1.7933995+01	-6.461510E-02	-1.045306E+01	2.653C20E+00	8.232379E+00	٠	00+147407F.4	5.25161F-01	1_834G67E+01	5.395935E+01	3.968146E+00	1.05:5466+01	3.6986966+00	-2.5219956+01	-2.540003E+01	-6.11£490E+01	4.215831E+02	6-417036E+01	-2.603683E+02	3.436512E+01
		8.363576E+01	-8.571990E+01	-6.116241E+02	-5.552952E+02	1.C65058E+00		Z. 3516598+01	1.6054825+03	1.628798E+02	6.726931E+01	2.956913E+01	7.6289985+01	1.6246916+62	-9.870543E-01	-1.155278E+02	10+1000001.1-	3-8520268401	6-572:556+51	-2.C579322+d2	-3_799994E+62	-6-664881E+01	-2.536543E+02	70+100+0043. III	COMMODUCACIÓN M	5.32373C+02	6.492626±01		- 1.331225E+02	-1.151957E+01	-1.722431E+02	-4.E32850E+C0	-1.C29916E+C1		では、はないのは、は、は、は、は、は、は、は、は、は、は、は、は、は、は、は、は、は、は、	いのようののののでは、は一	-3.E46843E-01	1.7051955+02	•	€ -2.2892245+01	-3.214435E+C1	8.5257305+61	6_120795E+01	-1.62523:E+62	-1.352217E+02	3.8774745+02	1.3447855+03	7_5075536+01
	¥	9.448358E+C1	1.287432E+02	-4.996442E+02	-4.023924E+02	-2.1e6111E+62	-1-339132E+04	-2-68:3772F+G2	-1,795377E+03	-6.262954E+02	-2.917098E+01	-5.472495E+02	5.457964E+01	1.41E886E+02	2.7.7482E+02	1.358798E+02	-4.57Z331E+01	-3-834422E+01	7.522645E+01	6.673439E+00	3.406083E+02	-1, 5-8560E+62	Z. 10/2/91+01	-8-50130E+02	ANTHONOUS AT A COLUMN TO C	-1 14R7F1F63	1.4493436+00	-7.635583E+C2	7.204536E+C1	-3.267305E+01	3.70685CE+60	6.3151945+01	-2.146325E+31	4,4807188401	10+4717977 · *-	-1 1784APF4C3	-1.1273685+62	-1.255 KBBE+C1	1.6790345+01	-3.253953E+01	-2.748393E+01	-1.224742E+02	-7.164911E+01	6-764237E+C1	-1.7575c3E+02	-6.311517E+02	-1.025417E+62	-7.251788E+01
	×	7.511792E+C0	-3.068325E+01	6.3308626+02	8-9260995+02	-5.673358E+01	- 2011167.7-		-2.7E2812E+03	-1.099943E+03	-1.398379E+01	-9.373641E+02	6.2617965+01	2.053544E+02	4.0192725+02	8-6563985+01	-267629E+	-1.2932455-12	3.4310878+01	5.1534726+02	1.6529795+03	-7.2453915+01	3.153403E+02	70+4007707-11	20+37:00:11-1-:	ADVECTOR TO THE	-3.0554716+01	-1.15C599E+03	1.9471556+52	3.2801716+01	1.0171456+02	2.3330335+01	-1.2671025+01	5.697354E+01	19430775(114	10-22-17-10-0-	20+9/90/04/1-	-1,339056E+62	-1.6587345+01	-1.200396E+62	-1.9093345+02	1.072722E+02	1.324210E+02	4.657313E+02	4.975863E+02	-1.4568705+03	.838056E+	1.012368E+02
	ID.	900006	900081	911400	912400	913587	001110	913000	916700	917800	918187	918500	919311	919332	919353	919375	97026	970937	1021287	1021400	1022400	1623587	1023700	1625600	1025087	1020700	1328187	1028900	1029311	1029353	1029375	100701	1040026	1040037	104004	1101201	1105887	1108187	1120011	1120037	1120053	1120400	1121400	1122400	1126700	1127800	1128900	1129311

RAIL HUMP-A/C END FORMARD-YERTICAL ACCELERATION UPMAGD

SUBCASE 1

	ě	æ	SSESIN	BAR ELE	2123	(CBAR)	3	
19.	3 13	. 285	7 S	588 584	STRESS	SB-KAX	NIM-BS	E.SC
200053	1.851646E+03 1.392094E+03	-9.846262E+C2 -6.345367E+02	-1.223014E+03 -8.968710E+02	1.347244£+03 8.295489E+02	-7.323654E+02	1.119341E+03 6.597882E+02	-1.952320E+03 -1.629176E+03	
200075	1.685844E+03 2.356794E+0\$	-8.376754E+02 -1.008514E+03	-1.100016E+03 -3.253141E+02	1.124593£+03 1.639579£+03	-6.303468E+02	1.056495E+Q3 1.069330E+O3	-1.730358E+03 -1.638862E+03	
200400	-2.734315E+03 5.309121E+03	-3.205905E+03 4.493539E+03	-3.205906E+03 4.493539E+03	5.002883E+03 -7.365627E+03	1.6183C2E+03	6.620885E+03 6.927121E+03	-1.537906E+03 -5.767627E+03	
231287	4.891426E+02 -1.090374E+03	-8.76:095E+C2 1.53:004E+03	-6.777066E+02 1.591950E+03	5.575028E+02 -1.613238E+03	-5.219590E+02	3.554380E+01 1.069991E+03	-1.398069E+03 -1.612333E+03	
201400	-9.225924E+03 3.916987E+03	-2.999565E+03 4.477603E+03	-2.999565E+03 4.477603E+03	6.366813E+63 -7.012192E+03	-2 <u>.</u> §33155E+02	6.103497E+03 4.214288E+03	-9.489239E+03 -7.275505E+03	
20250c	-1.116373E+04 9.038047E+02	-1.294127E+63 5.448131E+63	-1.294127E+03 5-448:31E+03	4.563214E+03 -7.555524E+03	-1.150515E+03	3.412698E+03 4.297616E+03	-1.231425E+04 -8.706039E+03	
203587	-1.539025E+03 -1.241865E+03	2.:81988E+03 2.042276E+03	2.242934E+03 1.755649E+03	-1.441583E+03 -1.316405E+03	4.382811E+01	2.286762E+03 2.086104E+03	-1.495197E+03 -1.272577E+03	
203800	-6.390721E+03 -6.927028E+02	7.925733E+C2 -9.373577E+C1	7.925739E+02 -9.373577E+01	5.500127E+02 3.012142E+02	-1.752862E+02	6.172877E+02 1.259283E+02	-6.566006E+03 -8.679690E+02	
205600	-5.525714E+02 6.627668E+03	6.457034E+62 -1.445226E+63	6.457534E+C2 -1.445226E+53	-7.256534E+02 2.67E326E+02	4.728457E+02	1.118549E+03 7.100513E+03	-2.558177E+02 -9.723802E+02	
205867	-1.147590E+03 -9.134263E+02	1.654530E+03 1.363262E+03	1.667152E+63 1.318068E+63	-1.689951E+03 -8.927686E+02	2.365771E+02	1.903729E+03 1.599839E+03	-9.110129E+02 -6.768492E+02	
206700	-7.837400E+02 6.928804E+33	-2.223299E+C3 1.383586E+C3	-3.223298E+03 1.363886E+03	4.533367E+03 -3.613111E+03	4.061341E+02	4.939201E+03 7.334939E+03	-2.817164E+03 -3.206977E+03	
207800	-4.003735E+63 1.728636E+03	-2.2147C2E+03 3.067266E+03	-2.214702E+03 3.067266E+03	3.990530E+03 -4.562146E+03	-9.270327E+02	3.063798E+03 2.140233E+03	-4.930768E+03 -5.489178E+03	
208187	-1.321494E+02 2.054771E+03	2.296448E+¢2 -2.820381E+¢3	1.6445005+52 -3.0124385+03	-1.467835E+C2 1.874195E+03	4.973274E+60	2.346181E+02 2.059744E+03	-1.418102E+02 -3.007464E+03	
208900	-6.836720E+03 5.749296E+03	2.766234E+03 1.829200E+03	2.7682345+C3 1.629200E+03	-1.994266E+03 -3.913755E+03	-8.270380E+02	1.5-1196E+03 4.922258E+03	-7.663758E+03 -4.740793E+03	
209386	0.0	Q.0 0.0	o-o	0.0	3.670341E+03	3.670341E+03 3.670341E+03	3.670341E+03 3.670341E+03	
219100	0.0	0.0	9 · 0 0 · 0	o.o o.o	-6.127751E+02	-6.127751E+02 -6.127751E+02	-6.127751E+02 -6.127751E+02	•

RAIL HUMP-A/C END FORMARD-VERTICAL ACCELERATION UPHARED

SUBCASE 1

1						; ;	:	
ELEMENT 10.	STRES FIBRE DISTANCE	S E S I N G I STRESSES : NGRMAL-X	ENERAL GORD IN ELEMENT COORD NORMAL-Y	U A D R I L A I D SYSTEM SHEAR-XY	E K A L FRINCI ANGLE	FLEEFENIS PALSTRESSES (ZERO WAJOR	RO SHEAR!	I MAX SHEAR
57800	0.0	-1.094442E+03 -1.094442E+03	-2.6:4827E+03_ -2.6:4827E+03	-2.205414E+03 -2.205414E+03	-35,4966 -35,4906	4.781202E+02 4.781202E+02	-4.187389E+03 -4.187389E+03	2.332755E+03 2.332755E+J3
58900	0.0	-1.045620E+02 -1.045620E+02	-1.500498E+02 -1.500498E+02	-1.938751E+C3	-44.6639 -44.6539	1.811578E+03 1.811578E+03	-2.066190E+03 -2.066190E+03	1.936884E+03, 1.938884E+03
119326	0.0	1.2911895+62 1.2911895+52	1.280238E+03	-2.543643E+03 -2.543643E+03	-5: .3744	3.312821E+03 3.312821E+03	-1.903464E+03 -1.903464E+03	2.608142E+03 2.608142E+03
119337	0.0	-1.939235E+02 -1.939235E+02	1.146375E+03 1.146375E+03	-2,446879E+03 -2,446879E+03	-52.6583 -52.6583	3.013215E+03 3.013215E+03	-2.060764E+03 -2.060764E+03	2.536990E+03 2.536990E+03
119353	0.0	5.935:81E+02 5.935:81E+02	8.977212E+C2 8.977212E+02	-1.4038285-03 -1.403828E+03	-48, 6909 -48, 6909	2.157708E+C3 2.157708E+O3	-6.663688E+02 -6.663688E+02	1.412038E+03 1.412038E+03
140011	0.0	-7.008364E+03 -7.008364E+03	-4.619043 <u>E+03</u> -4.619043 <u>E+</u> 03	-3.634997E+03 -3.634997E+03	-54, 0956 -54, 0956	-1.987320E+03 -1.987320E+03	-9.639787E+03 -9.639787E+03	3.826233E+03 3.826233E+03
140053	0.0	9.055479E+02 9.055479E+02	-1.C35516E+03 -1.C38516E+03	-1.083432E+02 -1.088432E+02	-3.1151	9.114714E+02 9.114714E+02	-1.094440E+03 -1.094440E+03	1.002955E+03 1.002955E+03
140075	0.0	3.090788E+03 3.090788E+03	8.002937E+01 8.032937E+01	4.268135E+02 4.263135E+02	7.9148	3.150126E+03 3.150126E+03	2.069061E+01 2.069061E+01	1.564718E+03 1.564718E+03
140400	0.0	-5.325845E+62 -5.325845E+02	-8.225179E+03 -8.225:79E+03	-3.128334E+03 -3.128334E+C3	-19.5614 -19.5614	5.789883E+02 5.789883E+02	-9.336752E+03 -9.336752E+03	4.957870E+03 4.957870E+03
141287	0.0	3.494642E+03 3.494642E+03	7.239581E+C2 7.239581E+02	6.651999E+02 8.651999E+02	15.9932 15.9932	3.742623E+03 3.742623E+03	4.759773E+02 4.759773E+02	1.633323E+03 1.633323E+03
141400	0.0	-2.705322E+63 -2.705322E+03	-6.465727E+03 -6.465727E+03	-3.719162E+03 -3.719162E+03	-31.5907 -31.5907	-4.181120E+02 -4.181120E+02	-8.752937E+03 -8.752937E+03	4.167413E+03 4.167413E+03
142500	0.0	-2.979570E+03 -2.979570E+03	-6.002742E+03 -6.002742E+03	-3.307046E+03 -3.307040E+03	-32.7182 -32.7182	-8.551011E+02 -8.551011E+02	-8.127311E+03 -8.127311E+03	3.636105E+03 3.636105E+03
143587	0.0	1.925598E+03 1.925598E+03	7.717483E+62 7.717483E+62	4.793162E+02 4.793102E+02	19,8599 19,8599	2.098727E+03 2.098727E+03	5.986194E+02 5.986194E+02	7.500536E+02 7.500536E+02
143800	0.0	-2.337368E+C3 -2.337366E+O3	-5.768:15E+C3 -5.768:15E+C3	-4.746035E+03 -4.746035E+03	-35.0642 -35.0642	9.937488E+02 9.937488E+02	-9.099232E+03 -9.099232E+03	5.046491E+03 5.046491E+03
145600	0.0	-2.101727E+33 -2.101727E+03	-4.370267E+03 -4.370267E+03	-4.608896E+03 -4.808896E+03	-38.3641	1.704859E+03 1.704859E+03	-8.176852E+03 -8.176852E+03	4.940855E+03 4.940855E+03
145887	0.0	1.302394E+03 1.302394E+53	6.420560E+02 6.420560E+02	5.589153E+02 5.589153E+02	29.7142 29.7142	1.621376E+03 1.621376E+03	3.230733E+02 3.230733E+02	6.491515E+02 6.491515E+02

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